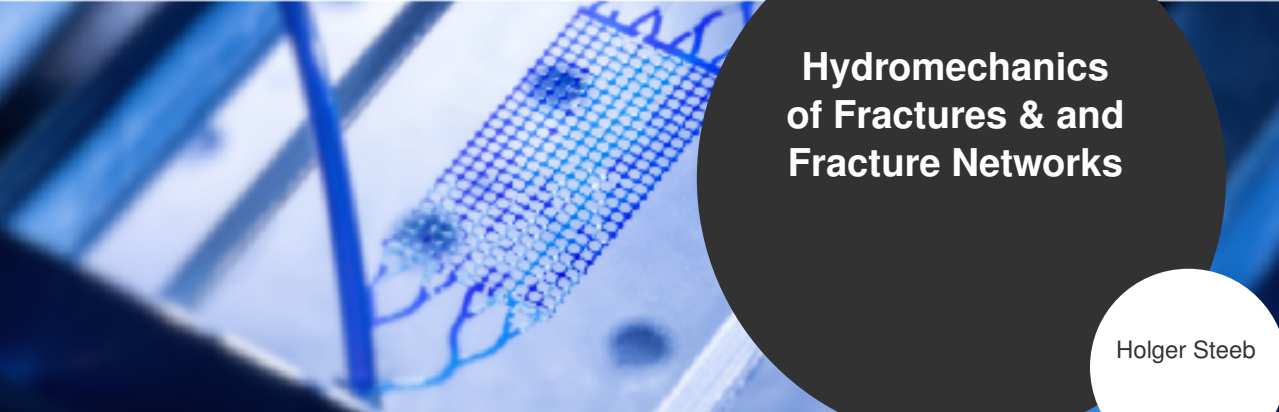




University of Stuttgart
Institute of Applied Mechanics



Hydromechanics of Fractures & and Fracture Networks

Holger Steeb



SFB 1313



P|M|L
Porous Media Lab

SimTech

Fracture characteristics

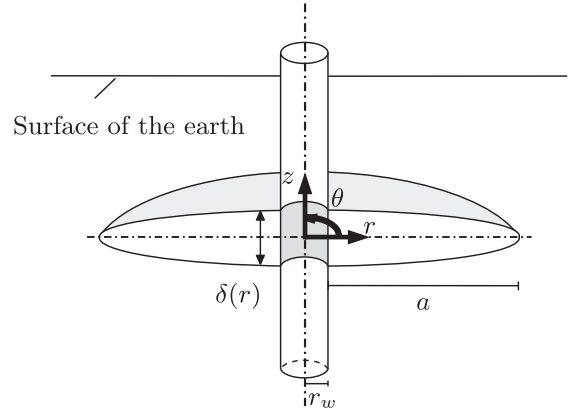
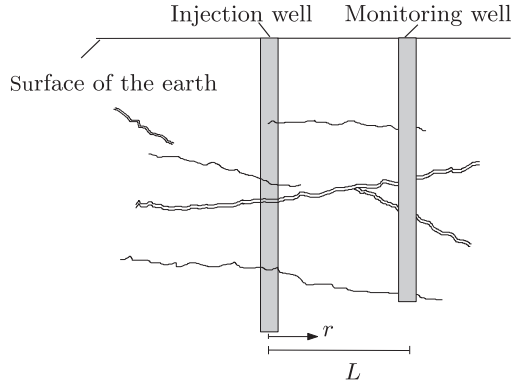
- aspect ratio: ratio of fracture length to fracture width $r_f = l/\delta$
- investigation of fractures with ratios $r_f \gg 10^5$
- transmissivity & storativity
- fractures embedded in matrix: hydro-mechanical coupling (inverse pressure response)

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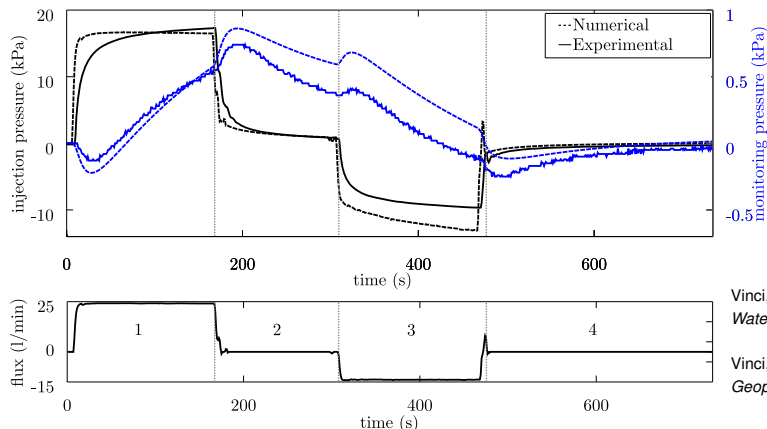


Fracture characteristics - typical borehole configuration



Numerical vs. experimental observations

- pressure evolution at injection borehole (black lines) & monitoring borehole (blue lines)
- numerical solutions (dashed lines) and field data (solid lines)
- vertical dashed lines: (1) injection, (2) pause, (3) production, and (4) pause



Vinci, Renner, Steeb (2014)
Water Resour. Res., **50**, 1616-1635

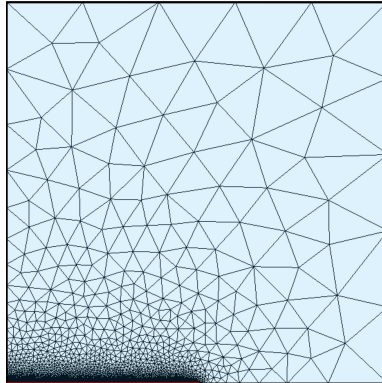
Vinci, Steeb, Renner (2015)
Geophys. J. Int., **200**, 1613-1626

Fracture characteristics - modelling issues

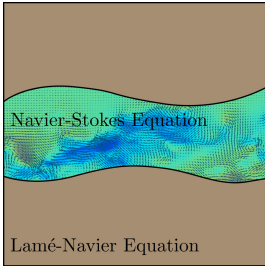
- coupling of governing PDEs (fracture - (poro)elastic matrix)
- aspect ratio of fracture leads to discretization problem for (D)irect (N)umerical (S)imulations (meshing, # of DOFs)
- coupling techniques of fracture and solid matrix needs to be identified

Fracture characteristics - modelling issues

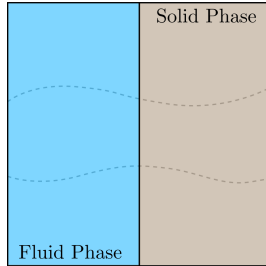
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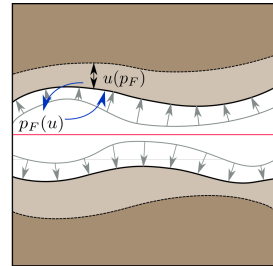
Modelling fractures - a matter of complexity



DNS



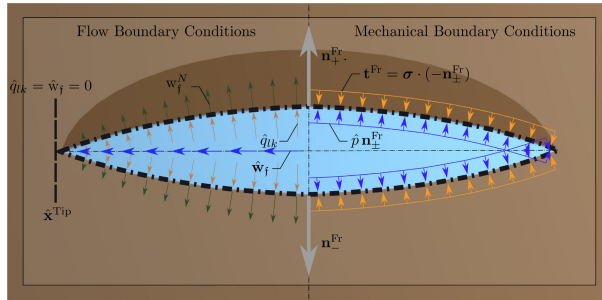
poroelastic approach



hybrid-dimensional

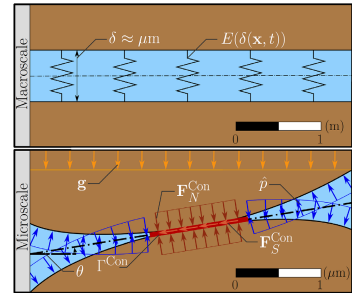
- strong coupling conditions at interface free flow - solid matrix
- fluid properties are not restricted (e.g. Re-number)
- efficient/necessary for e.g. discretizations with $r_f \ll 10^4$
- modeled with Biot's poroelastic equations
- coupling due to coarse-grained momentum interaction
- large defs. within fracture lead to extended formulations
- introduces a priori assumptions for fluid domain
- naturally covers large deformations within fractures (BCs)
- also efficient for high aspect ratios $r_f \gg 10^5$

Modelling fractures - a matter of complexity



... some modelling aspects (hybrid-dimensional approach)

- ❖ incl. effective fracture stiffness / effective stress concept
- ❖ leak-off effects (porous rock)
- ❖ deformable fracture & poro-elastic rock & fluid flow in fracture



Governing equation - hybrid-dimensional formulation

$$\frac{\partial p}{\partial t} - \left[\frac{\delta^2}{12 \eta^{fR}} \right] \left(\frac{\partial p}{\partial x} \right)^2 - \left[\frac{\delta}{12 \eta^{fR} \beta^f} \right] \frac{\partial p \partial \delta}{\partial x \partial x} - \left[\frac{1}{12 \eta^{fR} \beta^f} \right] \frac{\partial}{\partial x} \left(\delta^2 \frac{\partial p}{\partial x} \right) + \left[\frac{1}{\delta \beta^f} \right] \frac{\partial \delta}{\partial t} = \frac{w^{fR,N}}{\delta \beta^f}$$

1 transient

4 diffusion

2 quadratic (nonlinear)

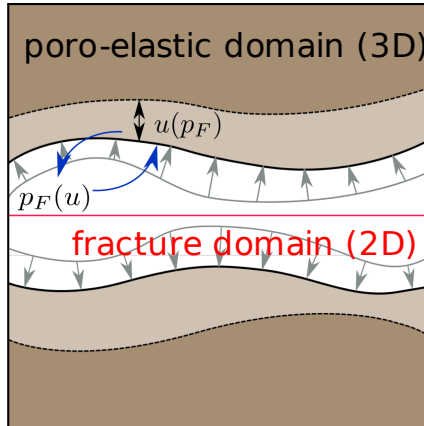
5 coupling

3 convection

Vinci, Renner, S. (2014) *Water Resour. Res.*, **50**, 1616-1635

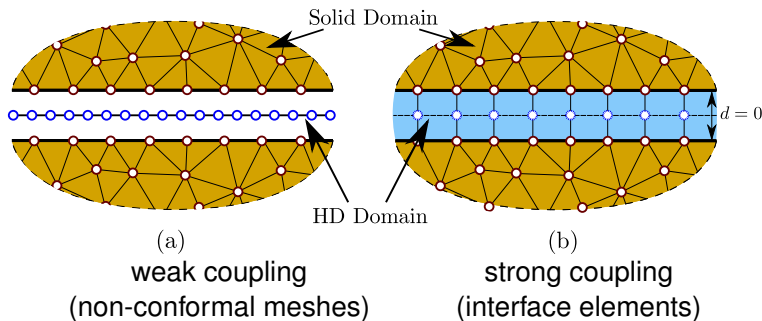
Governing equation - hybrid-dimensional formulation

How do we couple now the (3D) poro-elastic domain with the (2D) fractures?



Governing equation - hybrid-dimensional formulation

- FE approach: strong coupling vs. weak (staggered) coupling



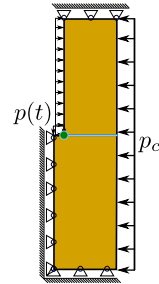
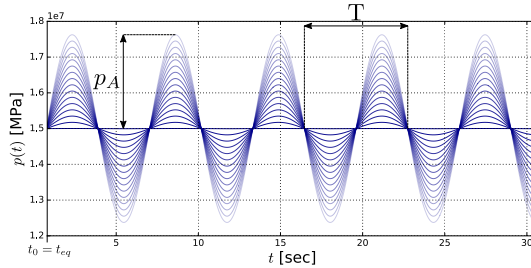
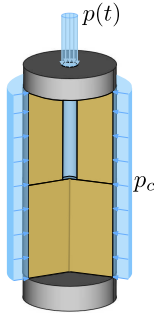
Schmidt, S. (2019) *Int. J. Geomath. (GEM)*, **10**, Doi:10.1007/s13137-019-0127-5

- FE approach: Biot's equations

Adachi et al. (2007) *Int. J. Rock Mech. Min. Sci.*, **44**, 739-757

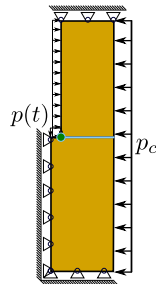
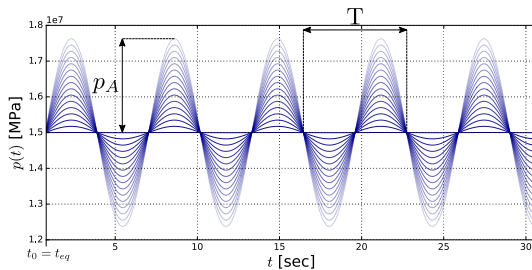
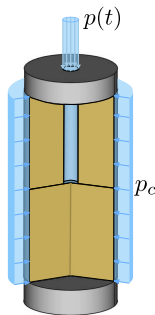
Segura (2008) *Int. J. Num. An. Met. Geom.*, **32**, 2083-2101

Modelling for **lab scale** experimental analysis



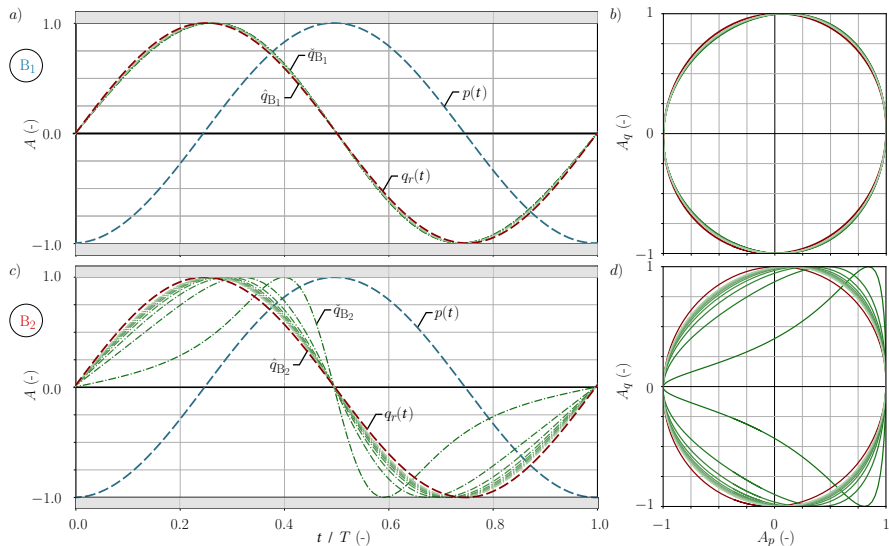
Modelling for **lab scale** experimental analysis

Schmidt, Steeb, Renner (2023)
Pure Appl. Geophys., **180**, 2841-2860

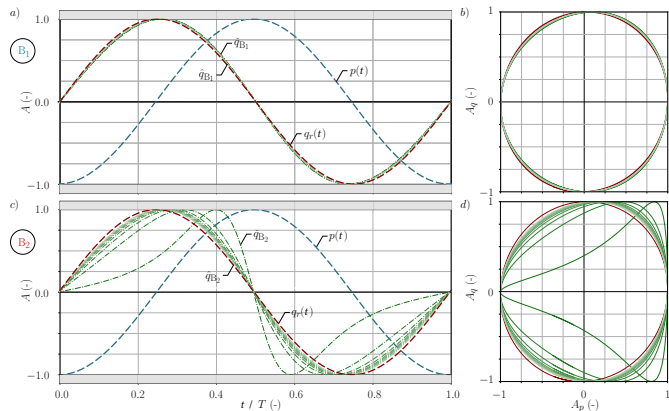


- sample dimension $r = 15$ mm, $h = 75$ mm
- equilibrium state for confining pressure (20 MPa) and constant upstream pressure (15.0 MPa)
- fracture stimulated by $p(t) = 15.0 \text{ MPa} - 2 \pi p_A \sin(t - t_{eq})$

Modelling for **lab scale** experimental analysis



Modelling for **lab scale** experimental analysis



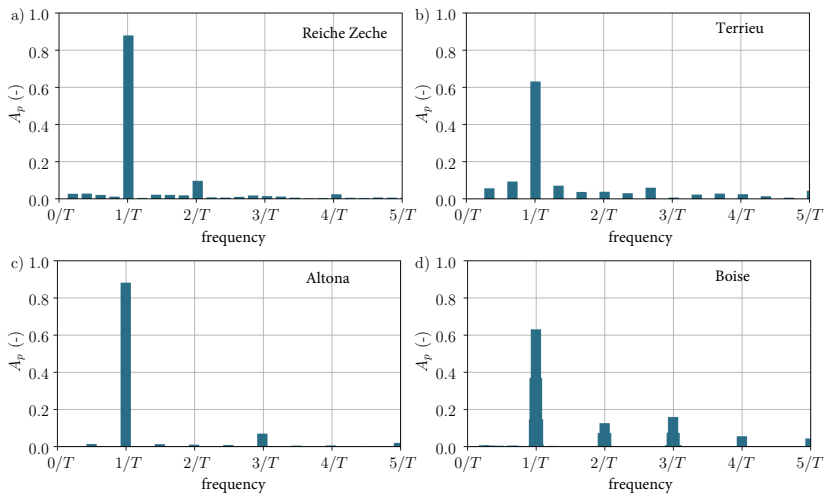
- large fracture deformations lead to **non-linear** relationship between pressure and flux
- permeability variations result in **non-constant pressure-flux phase shifts** within one period T

From **lab scale** (back) to **field scale**

Investigation of the records of (different) field studies that employed harmonic pumping

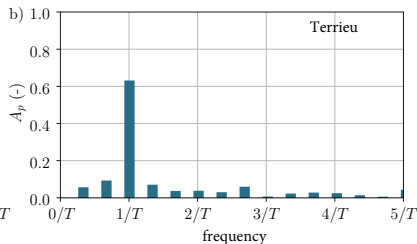
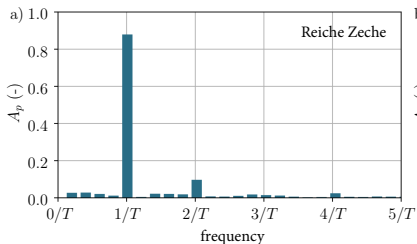
- **Reiche Zeche** underground-research laboratory (RZ), Freiberg, Germany (Renner et al., 2021)
- **Terrieu karstic field**, near Montpellier, France (Fischer et al., 2018)
- **Altona Flat Rock Site**, Clinton County, NY, USA (Guiltinan and Becker, 2015)
- **Boise Hydrogeophysical Research Site**, Boise, ID, USA (Rabinovich et al., 2015)

From lab scale (back) to field scale



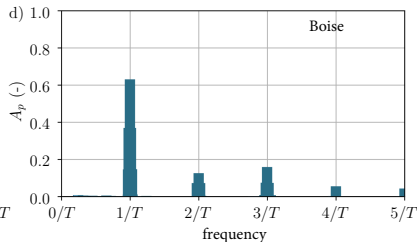
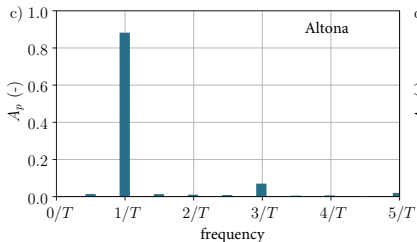
From lab scale (back) to field scale

(stiff) crystalline rock
gneiss



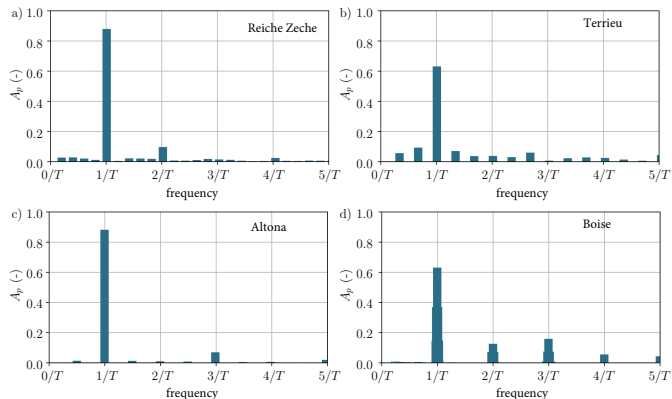
(soft) karstic rock

(stiff) sandstone



(soft) unconfined aquifer
sand / gravel

From lab scale (back) to field scale



- hydro-mechanical coupling (could) lead to distinct non-linear effects
- higher harmonics could be explained by non-linearities

take home message:

- * linear/non-linear hydro-mechanics of fractures

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- * harmonic (pumping) tests could lead to non-linearities & overtones

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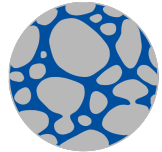
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- * modeling fractures could be complex
- * . . . but experimental characterization of fractures is also not trivial

take home message:

- * linear/non-linear hydro-mechanics of fractures
- * harmonic (pumping) tests could lead to non-linearities & overtones
- * modeling fractures could be complex
- * ... but experimental characterization of fractures is also not trivial
- * if you are interested - have a closer look at SFB 1313 & PML



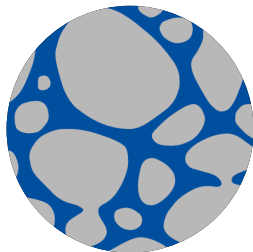
P|M|L





University of Stuttgart
Germany

Thank You!



Holger Steeb

E-Mail holger.steeb@mechbau.uni-stuttgart.de

Phone +49 711 685-66346

Fax +49 711 685-66347

University of Stuttgart
Institute of Applied Mechanics (MIB)
Collaborative Research Center SFB 1313
Stuttgart Center of Simulation Science (SC SimTech)
70569 Stuttgart