

Using In-situ Wettability Measurements to Reconstruct the Wetting Condition of a Natural Rock

Ruichang Guo¹, Laura E. Dalton², Hongsheng Wang¹, James McClure¹, Dustin Crandall², Cheng Chen³

¹ VIRGINIA TECH
 ² NATIONAL ENERGY TECHNOLOGY LABORATORY
 ³ STEVENS INSTITUTE OF TECHNOLOGY

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- **1.** Objective
- 2. Review on wettability heterogeneity model
- **3.** Modeling and reconstructing heterogeneous wettability
- 4. Implications on immiscible displacement
- **5.** Summary





- □ In-situ measurements of wettability on natural rocks published recently suggest that wettability heterogeneity of a natural rock is at a subpore scale and wettability has a wide range.
- This work is to model the heterogeneous wettability based on in-situ wettability measurements on a Bentheimer sandstone and explore the implications of pore-scale wettability heterogeneity on immiscible displacement in a sandstone.



2. Review on Wettability Heterogeneity Model



Literature review on wettability heterogeneity model of a porous medium

Studies	Porous media	Porous media Fluids Method		Surface wettability
(Bakhshian and Hosseini 2019)	Tuscaloosa sandstone	Tuscaloosa sandstone Brine/CO ₂ LB modeling		Fractional wet
(Maziar Arshadi 2020)	Arkose	N/A ¹	Experiment and pore network modeling	Fractional wet
(Zhao et al. 2018)	Computer-generated solid spheres	N/A	LB modeling	Fractional wet
(Landry et al. 2014)	Glass and polyethylene bead packs	Brine/kerosene	Experiment and LB modeling	Mixed wet
(Hwang et al. 2006)	Mixture of quartz sand and organosilane- treated sand	Water/oil	Experiment	Fractional wet
(Masalmeh 2003)	Carbonate	Water/oil	Experiment	Mixed wet
(Bradford and Leij 1995)	Mixture of octadecyltrichlorosilane-treated and untreated sandsWater/air, water/oil, and water/ail/oilExperiment		Experiment	Fractional wet

Water-wet grains

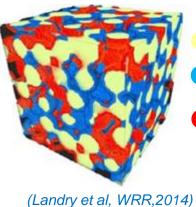
Water

Air

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Non-water- wet grains





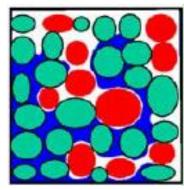
4/14

Solid

Water wet surface

Non-water wet surface

Fractional wet



(Hwang et al. AWR, 2006)

Fractional wet



) Water-wet

Non-water-wet

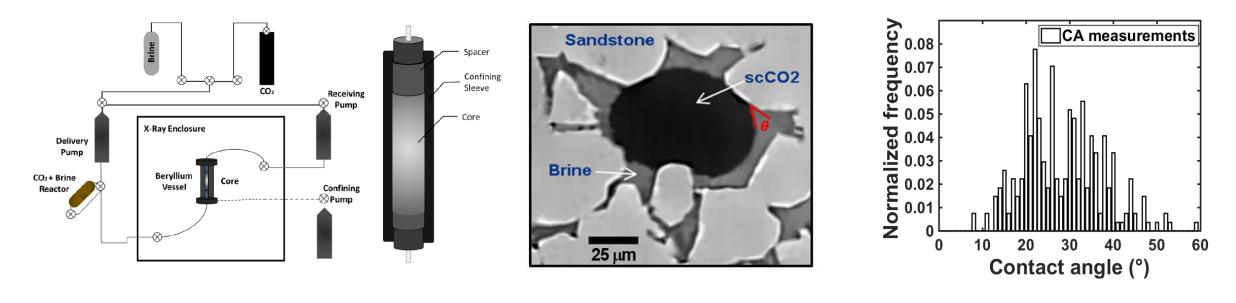
Pore space

(Bakhshian et al, AWR, 2019) VIRGINIA

3. Modeling Wettability Heterogeneity

3.1 In-situ measurements of wettability

The core flooding experiment and X-ray micro-CT imaging were performed at U.S. Department of Energy (DOE)'s National Energy Technology Laboratory (NETL).



Core flooding experiment setup

Schematic diagram on contace angle measurement

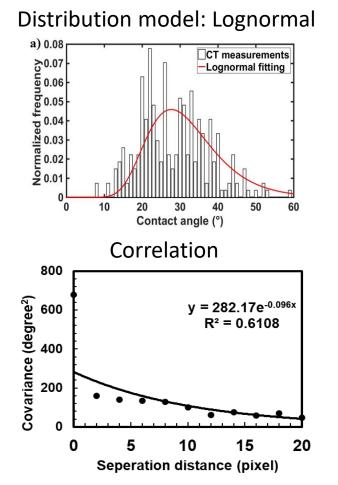
Distribution of contact angles



3. Modeling Wettability Heterogeneity

3.2 Model heterogeneous wettability as a random field

Model



6/14

Generation

Lognormal assumption:

 $Y \sim N(\mu_Y, \sigma_Y^2)$ $Y = \log(\theta)$

Correlation matrix decomposition:

 $c_{Y}(\mathbf{x},\mathbf{y}) = \sigma_{Y}^{2} \exp\left[-\left(|x_{1}-y_{1}|/L_{1}+|x_{2}-y_{2}|/L_{2}+|x_{3}-y_{3}|/L_{3}\right)\right]$ $c_{Y}(\mathbf{x},\mathbf{y}) = \sum_{n=1}^{\infty} \lambda_{n} \psi_{n}(\mathbf{x}) \psi_{n}(\mathbf{y})$

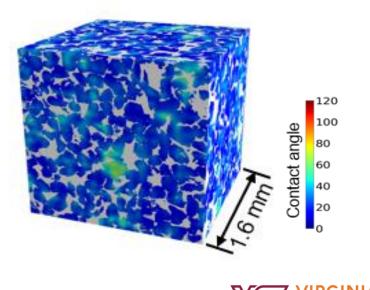
Generate Y field:

$$\mathbf{Y}(\mathbf{x}) = \langle \mathbf{Y}(\mathbf{x}) \rangle + \sum_{n=1}^{\infty} \xi_n \sqrt{\lambda_n} \psi_n(\mathbf{x})$$

Karhunen-Loève expansion

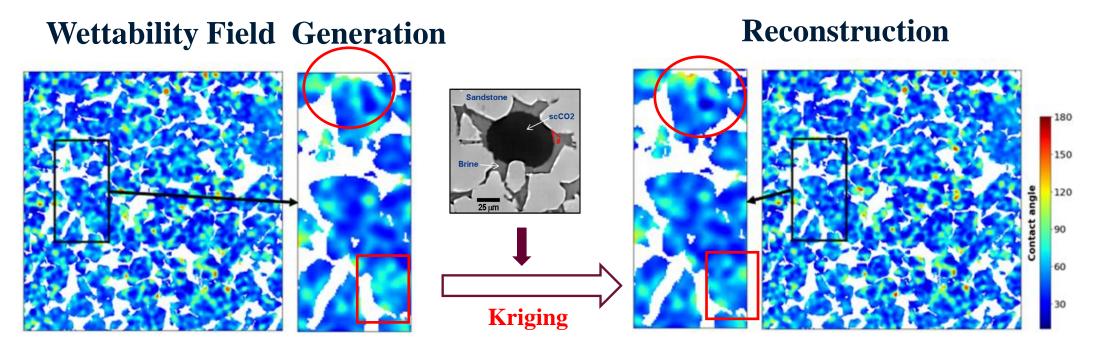
Wettability construction

- Convert the Y field into a θ field
- Mapping the θ field onto the Bentheimer sandstone



3. Modeling Wettability Heterogeneity

3.3 Reconstruction of heterogeneous wettability



Wettability field generation

Conditioned wettability field with measured CAs

$$Y_{cs}\left(\mathbf{x}\right) = Y_{us}\left(\mathbf{x}\right) + Y_{SK}\left(\mathbf{x}\right) - Y_{SK,us}\left(\mathbf{x}\right)$$

- Y_{cs} Conditional wettability field Y_{SK} Wettability field kriged from measured wettability Y_{us} Unconditional wettability $Y_{SK,us}$ Wettability kriged from simulated wettability \bigvee
 - Unity

7/14

4.1 Generated hterogeneous wettability models

The investigations were conducted in the context of geological carbon sequestration.

Wettability classification in a CO₂-Brine-Rock system

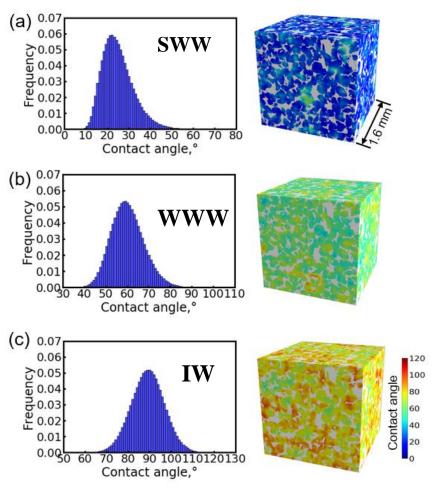
Strongly water-we		Veakly ater-wet	Intermeidate wet	Weakly CO ₂ -wet	Strongly CO ₂ -wet
0°	50°	7(D° 110)° 13	30° 180°
	o			(Ig	lauer et al., 2015)

Wettability field generation

- Method: Karhunen-Loève expansion (KLE)
- Stotistical parameters: Standard deviation, 9° Correlation length, 118.6 μm

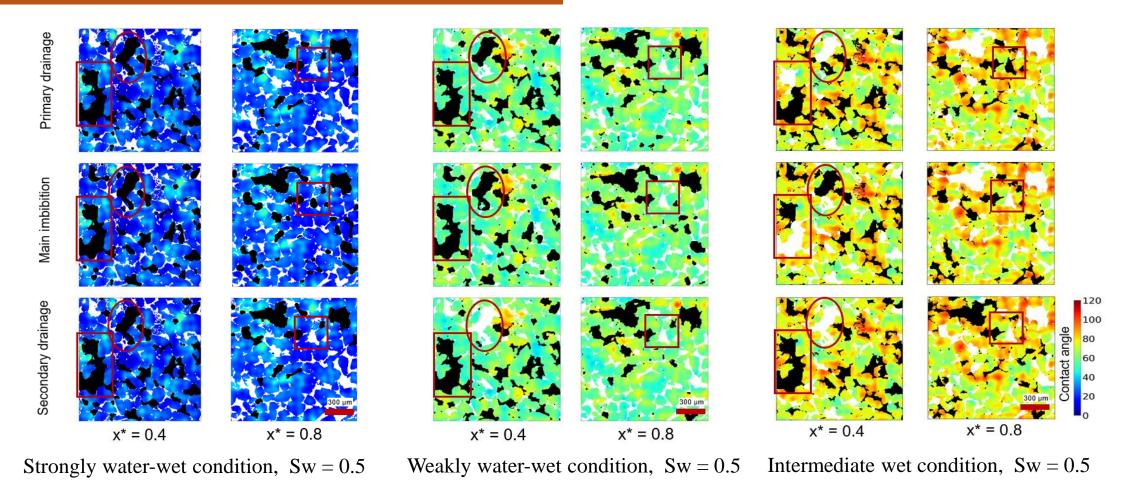
Direct simulation

- Color-gradient LB multiphase model
- Hybrid, multicore CPU/GPU parallel computing



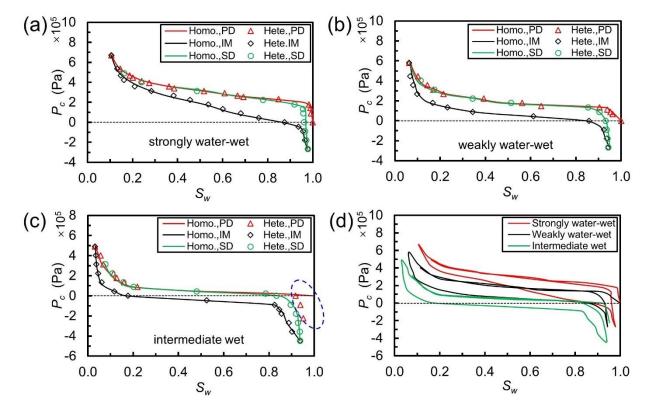


4.2 Impact on scCO₂/water configuration



4.3 Impact on Pc-Sw curve

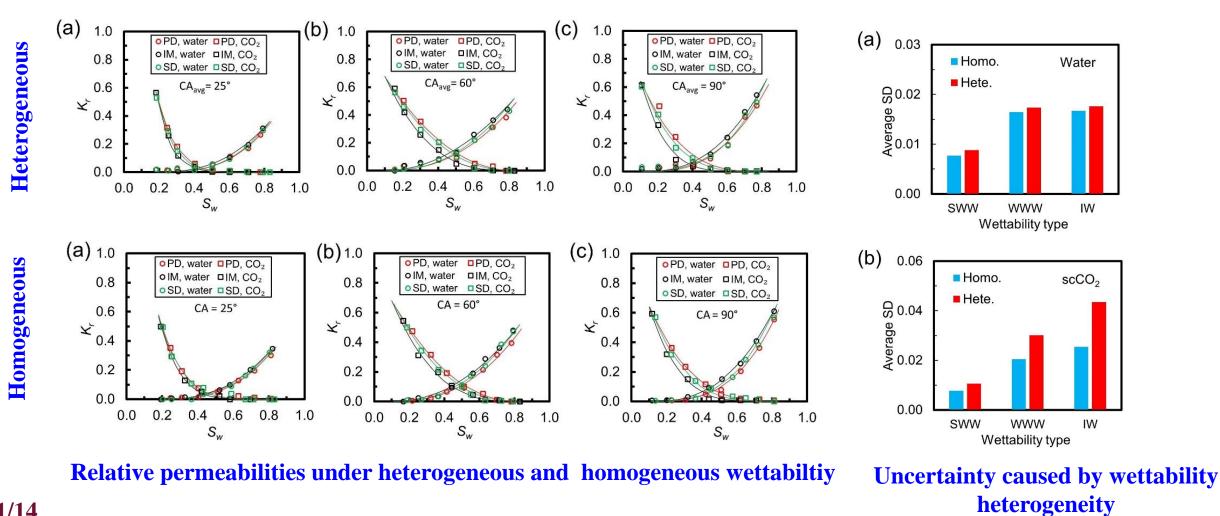
- The Pc-Sw curves for homogeneous and heterogeneous wetting condition are consistent.
- Pore-scale heterogeneity effects on local redistribution of scCO₂/water plumes are averaged out on macroscopic *PC-Sw* curve.
- Under homogeneous IW condition, the entry pressure for PD path is zero;
- Under heterogeneous IW condition, the entry pressure for PD path is negative.



To ensure the accuracy, enough timesteps are simulated. The average total time step for each case is 3.12×10^8 .



4.4 Impact on relative permeability



11/14

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□ Summary

- □ In-situ measurements of wettability confirmed that wettability of a natural rock was heterogeneous at a subpore scale. The wettability followed a lognormal distribution.
- □ Pore-scale wettability heterogeneity does not cause noticeable impact on *Pc-Sw* curve, except that under the heterogeneous IW condition, the entry pressure of the PD stage was negative, whereas it was zero under the homogeneous IW condition.
- □ Pore-scale wettability heterogeneity causes noticeable uncertainty in relative permeabilities.



□ Acknowlegements

□ The authors are thankful to the financial support provided by the U.S. Department of Energy (DOE)'s National Energy Technology Laboratory (NETL), and the support of supercomputers from Virginia Tech's Advanced Research Computing.

Reference

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- Guo, R., et al. (2022). Role of heterogeneous surface wettability on immiscible displacement, capillary pressure, and relative permeability in a CO2-brine-rock system. Advances in Water Resources, in press.
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 13/14



Thank you!



14/14

Research plan

Comprehensive sensitivity analysis to study the respective and combined effects of standard deviation and correlation length of surface CAs.

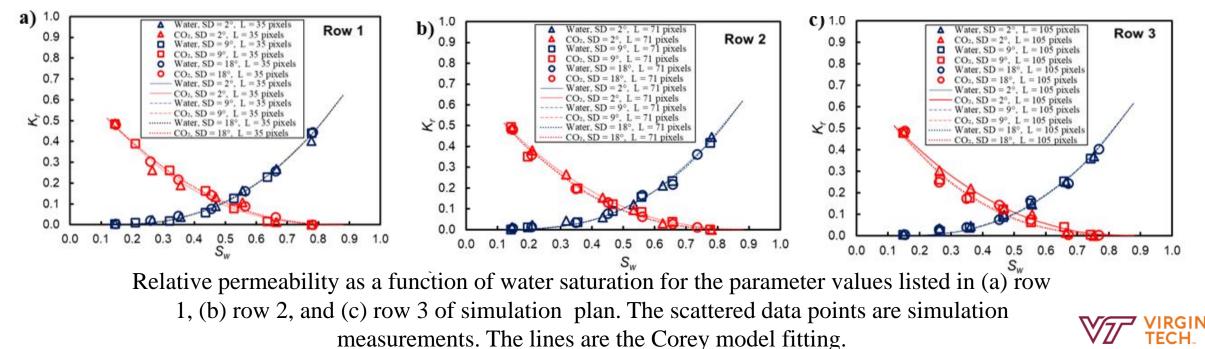
$ \begin{array}{c} \mu_{Y} = 3.3623, \sigma_{Y} = 0.1000; \\ \mu_{\theta} = 29^{\circ}; \sigma_{\theta} = 2^{\circ}; \\ L = 35 \text{pixels} \end{array} $	$\mu_{Y} = 3.3213, \ \sigma_{Y} = 0.3033;$ $\mu_{\theta} = 29^{\circ}, \ \sigma_{\theta} = 9^{\circ};$ L = 35 pixels	μ_{Y} = 3.2044; σ_{Y} = 0.5709 μ_{θ} = 29°, σ_{θ} = 18°; L = 35 pixels
μ_{Y} = 3.3623, σ_{Y} =0.1000;	μ_{Y} = 3.3213, σ_{Y} = 0.3033;	μ_{Y} = 3.2044; σ_{Y} = 0.5709;
μ_{θ} = 29 °, σ_{θ} = 2°;	μ_{θ} = 29°, σ_{θ} = 9°;	μ_{θ} = 29°, σ_{θ} = 18°;
L = 71 pixels	L = 71 pixels	L = 71 pixels
μ_{Y} = 3.3623, σ_{Y} =0.1000;	μ_{Y} = 3.3213, σ_{Y} = 0.3033;	μ_{Y} = 3.2044; σ_{Y} = 0.5709;
μ_{θ} = 29 °, σ_{θ} = 2°;	μ_{θ} = 29°, σ_{θ} = 9°;	μ_{θ} = 29°, σ_{θ} = 18°;
L = 105 pixels	L = 105 pixels	L = 105 pixels



□ Results_Impact of SD on relative permeability

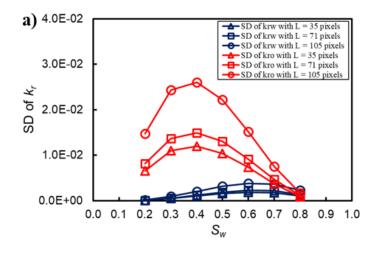
A.2

- The SD affects the relative permeability of scCO₂ more than water. Water flow along surface, insensitive to wettability heterogeneity compared to CO₂.
- The SD affects the relative permeability of scCO₂ and water in the middle of saturation axis than ends. When water saturation is in (0.3, 0.7), scCO₂ distribution is scattered, resulting uncertainty in relative permeability.

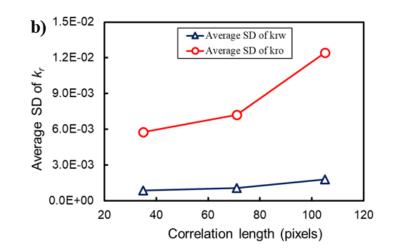


□ Results_Impact of SD on relative permeability

- The " Λ " shape relation between SD of kr and Sw clearly demonstrates that impact: scCO₂>water, middle > ends.
- \succ Larger *L* leads to larger *SD* of *kr*.



SD between the Corey-model-fitted *kr* values due to the variation in SD of CA as a function of Sw.



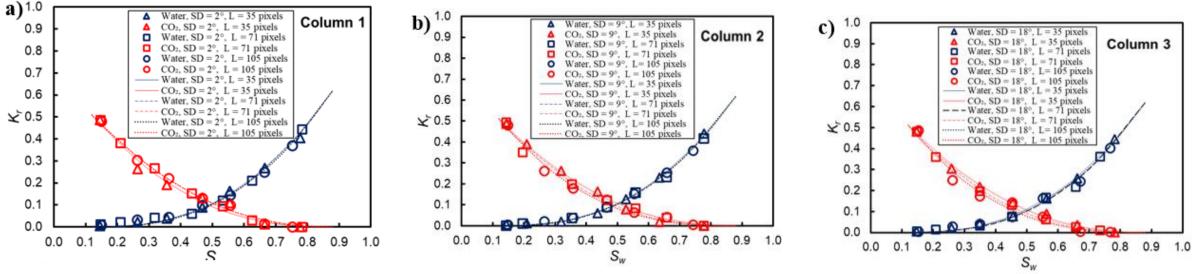
Average SD between the Corey-model-fitted k_r curves as a function of the *L*.



□ **Results_Impact** of *L* on CO₂/water configuration

A.4

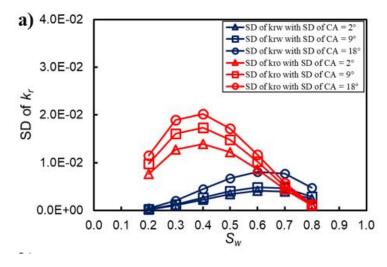
- The *L* affects the relative permeability of $scCO_2$ more than water. Water flow along surface, insensitive to wettability heterogeneity compared to CO_2 .
- > The *L* affects the relative permeability of $scCO_2$ and water in the middle of saturation axis than ends. When water saturation is in (0.3, 0.7), $scCO_2$ distribution is scattered, resulting uncertainty in relative permeability.



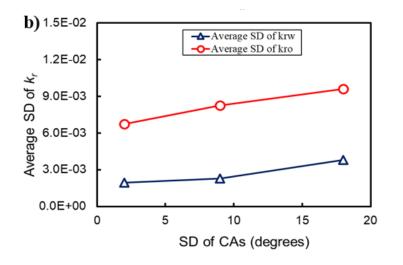
Relative permeability as a function of water saturation for the parameter values listed in (a) column 1, (b) column 2, and (c) column 3 of simulation plan. The scattered data points are simulation measurements. The lines are the Corey model fitting.

□ **Results_Impact** of *L* on CO₂/water configuration

- The " Λ " shape relation between SD of kr and Sw clearly demonstrates that impact: scCO₂>water, middle > ends.
- \succ Larger SD leads to larger SD of kr.



SD between the Corey-model-fitted kr values due to the variation in L of CA as a function of S_w .



Average *SD* between the Corey-model-fitted k_r curves as a function of the *SD*.

