Tightly Coupled Hyperbolic Treatment of Buoyant Two-Phase Flow and Transport in Porous Media

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tightly coupled, explicit flow and transport scheme for natural convection of multiple phases which is suited for computations on GPUs





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Problem and Motivation:

fully implicit methods are expensive and sequential methods require small time steps due to tight coupling between flow and transport



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coupled hyperbolic system for flow and transport based on augmented isothermal Euler equations with source terms explicit time integration using an approximate Riemann solver





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Method:

coupled hyperbolic system for flow and transport based on augmented isothermal Euler equations with source terms explicit time integration using an approximate Riemann solver high order in space and time

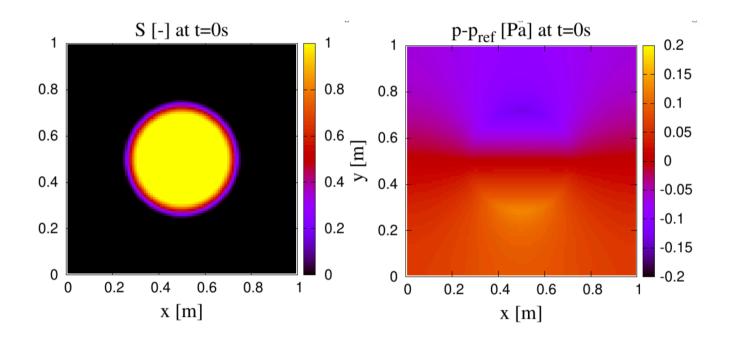
Results:

demonstration of accuracy and computational efficiency for 1D and 2D test cases with natural convection





Motivation

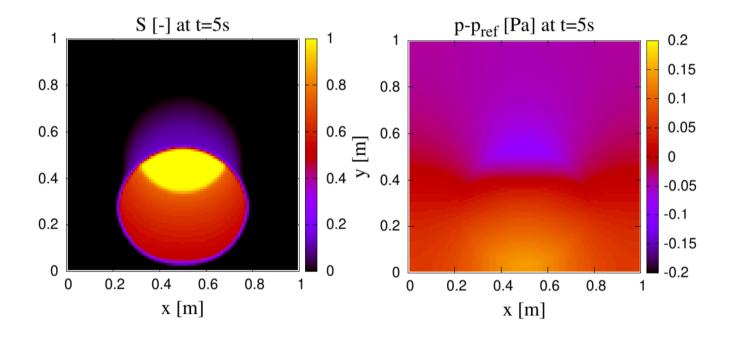




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Motivation

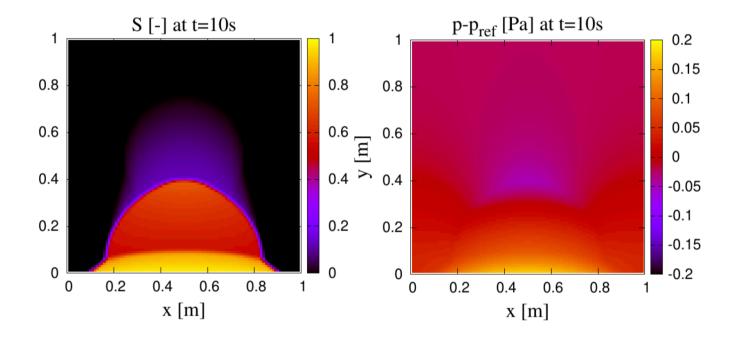




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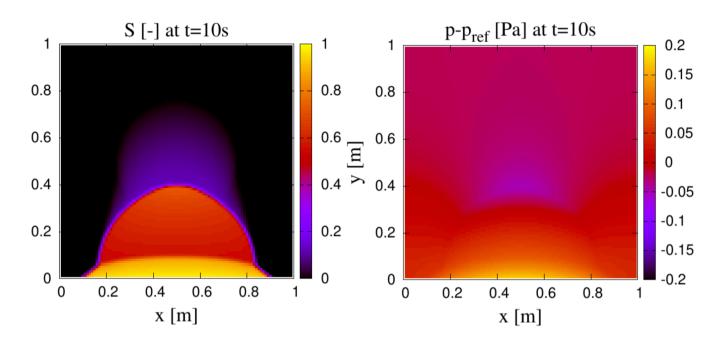


Motivation







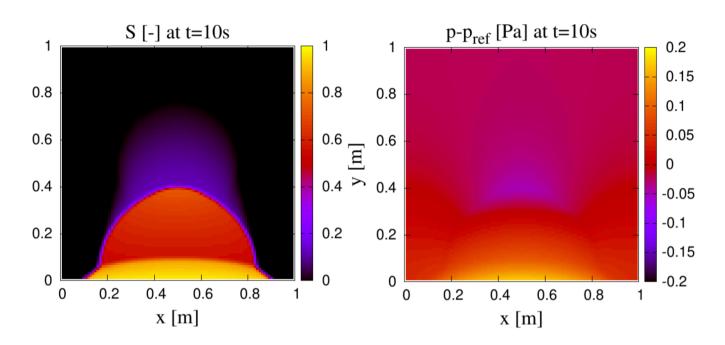


$$\nabla \cdot \boldsymbol{u} = 0$$

$$\boldsymbol{\uparrow}$$

$$\boldsymbol{u} = -\lambda k \nabla p + k \gamma \boldsymbol{g}$$





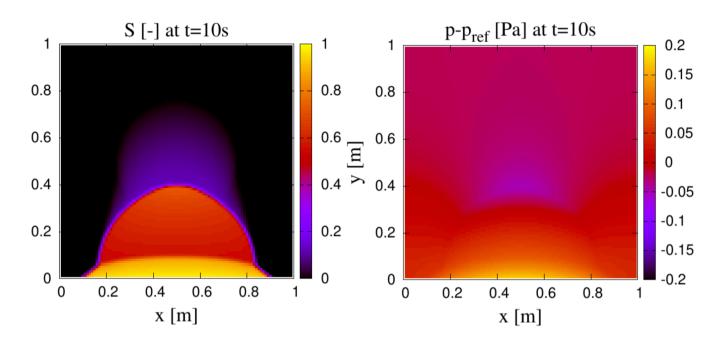
$$\nabla \cdot \boldsymbol{u} = 0$$

$$\boldsymbol{u} = -\lambda k \nabla p + k \gamma \boldsymbol{g}$$

$$\lambda = \frac{k_{r_{p1}}}{\mu_{p1}} + \frac{k_{r_{p2}}}{\mu_{p2}} \text{ and } \gamma = \lambda_{p1} \rho_{p1} + \lambda_{p2} \rho_{p1}$$

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$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g}$$

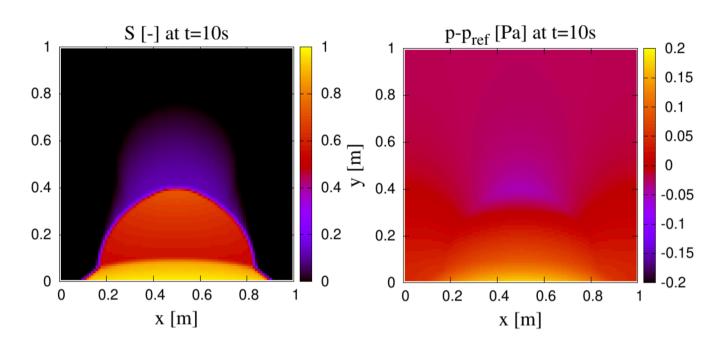
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$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g}$$

$$f_1(S) = \frac{\lambda_{p1}(S)}{\lambda(S)} \text{ and } f_{12}(S) = \frac{\lambda_{p1}(S)\lambda_{p2}(S)}{\lambda(S)} (\rho_{p1} - \rho_{p2})k$$

$$\nabla \cdot \boldsymbol{u} = 0$$

$$\boldsymbol{u} = -\lambda k \nabla p + k \gamma \boldsymbol{g}$$

$$\lambda = \frac{k_{r_{p1}}}{\mu_{p1}} + \frac{k_{r_{p2}}}{\mu_{p2}} \text{ and } \gamma = \lambda_{p1} \rho_{p1} + \lambda_{p2} \rho_{p2}$$





$$\frac{\partial}{\partial t} \underbrace{\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho Y \end{pmatrix}}_{U} + \frac{\partial}{\partial x} \underbrace{\begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho u v \\ F_{x}^{Y} \end{pmatrix}}_{R_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho v u \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$

$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0 \qquad \nabla \cdot \boldsymbol{u} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g} \qquad \boldsymbol{u} = -\lambda k \nabla \boldsymbol{u}$$

$$\begin{array}{rcl}
\mathbf{v} \cdot \mathbf{u} &=& 0 \\
& & \\
\mathbf{u} &=& -\lambda k \nabla p + k \gamma \mathbf{g}
\end{array}$$





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$$\frac{\partial}{\partial t} \underbrace{\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho Y \end{pmatrix}}_{U} + \frac{\partial}{\partial x} \underbrace{\begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho u v \\ F_{x}^{Y} \end{pmatrix}}_{F_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho v u \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$

$$\mathbf{R} = -\frac{1}{\lambda k}\mathbf{u} + \frac{\gamma}{\lambda}\mathbf{g}$$

$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g}$$

$$\nabla \cdot \boldsymbol{u} = 0$$

$$\boldsymbol{u} = -\lambda k \nabla p + k \gamma \boldsymbol{g}$$

$$\frac{\partial}{\partial t} \underbrace{\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho Y \end{pmatrix}}_{U} + \frac{\partial}{\partial x} \underbrace{\begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho uv \\ F_{x}^{Y} \end{pmatrix}}_{F_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho vu \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$

$$R = -\frac{1}{\lambda k} u + \frac{1}{\lambda k} u + \frac{1}{\lambda k} \underbrace{\begin{pmatrix} \rho v \\ \rho vu \\ F_{x}^{Y} \end{pmatrix}}_{F_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho vu \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$

$$\mathbf{R} = -\frac{1}{\lambda k}\mathbf{u} + \frac{\gamma}{\lambda}\mathbf{g}$$

$$Y = \phi S$$

$$\mathbf{F}^{Y} = \rho \mathbf{u}_{p1}$$

$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g}$$

$$\begin{array}{rcl}
\nabla \cdot \boldsymbol{u} &=& 0 \\
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$$\frac{\partial}{\partial t} \underbrace{\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho Y \end{pmatrix}}_{U} + \frac{\partial}{\partial x} \underbrace{\begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho u v \\ F_{x}^{Y} \end{pmatrix}}_{F_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho v u \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$

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if the following numbers are small:

- the maximum relative density variation $\Delta \hat{\rho}_{max} = (\rho_{max} \rho_{min})/\rho_{mean}$
- the dimensionless number $\mathcal{R} = \rho \lambda k |\mathbf{u}| / L_{flow}$, and
- the Mach number $Ma = |\mathbf{u}|/c$

$$\frac{\partial \phi S}{\partial t} + \nabla \cdot \boldsymbol{u}_{p1} = 0$$

$$\boldsymbol{u}_{p1} = f_1 \boldsymbol{u} + f_{12} \boldsymbol{g}$$

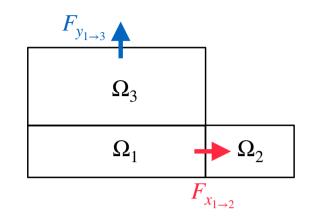
$$\nabla \cdot \boldsymbol{u} = 0$$

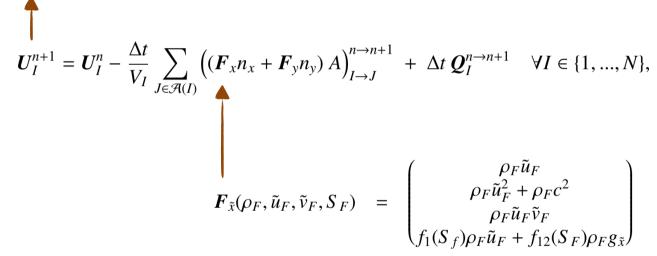
$$\boldsymbol{u} = -\lambda k \nabla p + k \gamma \boldsymbol{g}$$





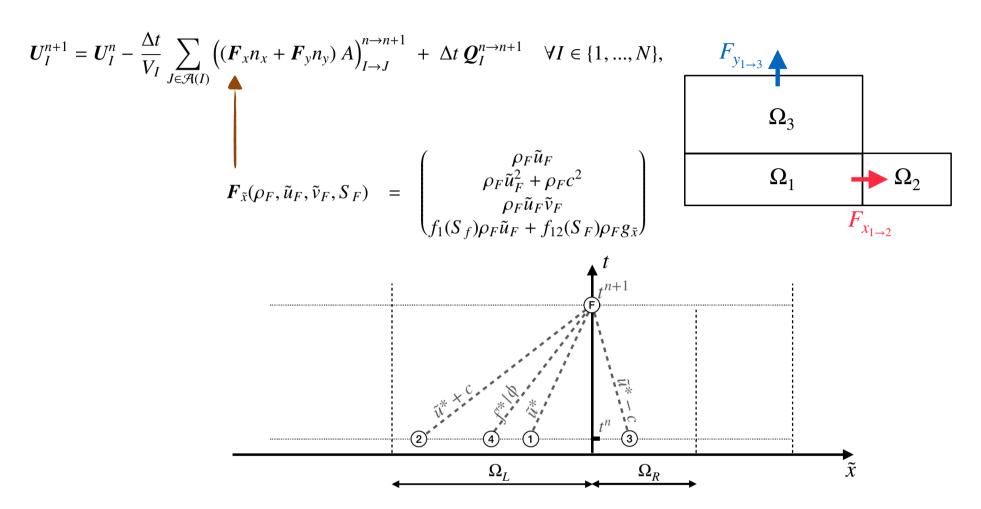
$$\frac{\partial}{\partial t} \underbrace{\begin{pmatrix} \rho \\ \rho u \\ \rho v \\ \rho Y \end{pmatrix}}_{U} + \frac{\partial}{\partial x} \underbrace{\begin{pmatrix} \rho u \\ \rho u^{2} + p \\ \rho u v \\ F_{x}^{Y} \end{pmatrix}}_{F_{x}} + \frac{\partial}{\partial y} \underbrace{\begin{pmatrix} \rho v \\ \rho v u \\ \rho v^{2} + p \\ F_{y}^{Y} \end{pmatrix}}_{F_{y}} = \underbrace{\begin{pmatrix} 0 \\ R_{x} \\ R_{y} \\ 0 \end{pmatrix}}_{Q}$$





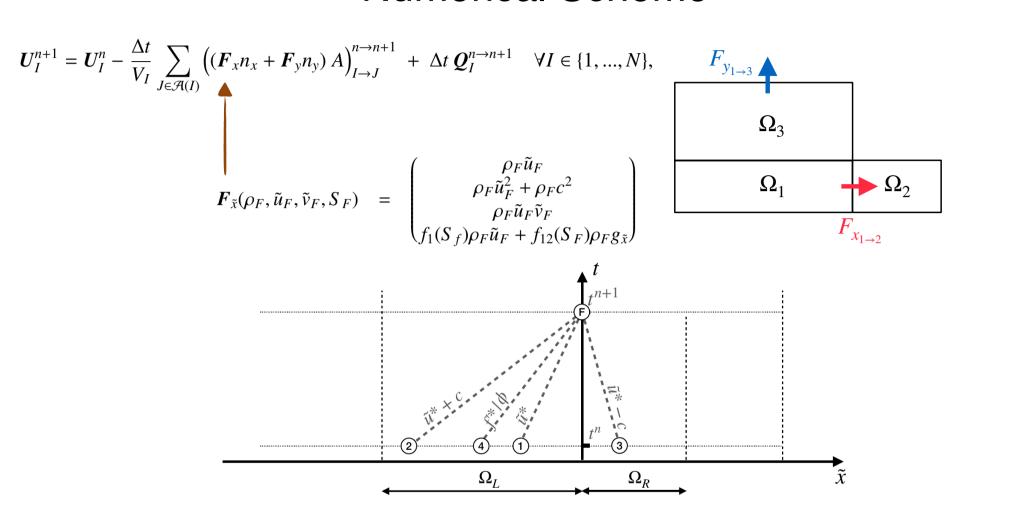
$$F_{\tilde{x}}(\rho_F, \tilde{u}_F, \tilde{v}_F, S_F) = \begin{pmatrix} \rho_F \tilde{u}_F \\ \rho_F \tilde{u}_F^2 + \rho_F c^2 \\ \rho_F \tilde{u}_F \tilde{v}_F \\ f_1(S_f) \rho_F \tilde{u}_F + f_{12}(S_F) \rho_F g_{\tilde{x}} \end{pmatrix}$$











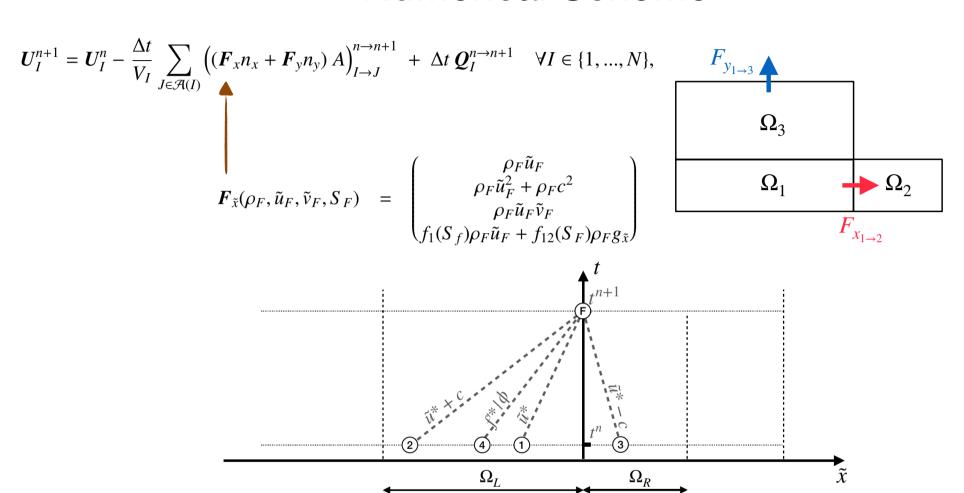
 $d\tilde{v} = 0$ along the characteristic wave with speed \tilde{u}^* ,

 $\rho^* d\tilde{u} + c d\rho = 0$ along the characteristic wave with speed $\tilde{u}^* + c$,

 $\rho^* d\tilde{u} - c d\rho = 0$ along the characteristic wave with speed $\tilde{u}^* - c$ and

 $\mathcal{A}d\rho + \mathcal{B}d\tilde{u} + CdS = 0$ along the characteristic wave with speed f'^*/ϕ ,





$$(\tilde{v}_{F} - \tilde{v}_{1}) = 0,$$

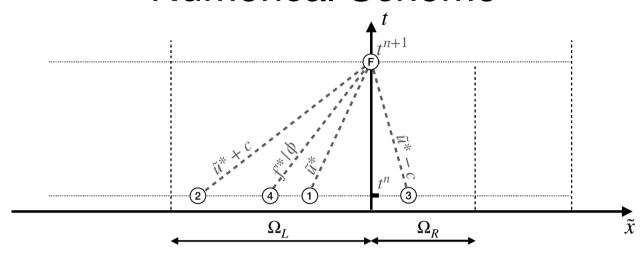
$$\rho^{*} (\tilde{u}_{F} - \tilde{u}_{2}) + c (\rho_{F} - \rho_{2}) = 0,$$

$$\rho^{*} (\tilde{u}_{F} - \tilde{u}_{3}) - c (\rho_{F} - \rho_{3}) = 0 \text{ and}$$

$$\mathcal{A}^{*} (\rho_{F} - \rho_{4}) + \mathcal{B}^{*} (\tilde{u}_{F} - \tilde{u}_{4}) + C^{*} (S_{F} - S_{4}) = 0.$$

along the characteristic wave with speed \tilde{u}^* , along the characteristic wave with speed $\tilde{u}^* + c$, along the characteristic wave with speed $\tilde{u}^* - c$ and along the characteristic wave with speed f'^*/ϕ ,





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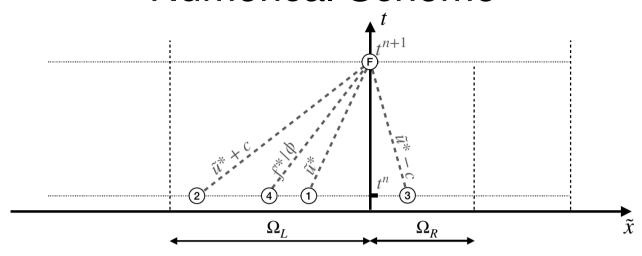
$$\rho^{*} (\tilde{u}_{F} - \tilde{u}_{3}) - c (\rho_{F} - \rho_{3}) = 0 \text{ and}$$

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along the characteristic wave with speed \tilde{u}^* , along the characteristic wave with speed $\tilde{u}^* + c$, along the characteristic wave with speed $\tilde{u}^* - c$ and along the characteristic wave with speed f'^*/ϕ ,

$$\tilde{v}_{F} = \tilde{v}_{1},$$
 $\tilde{u}_{F} = (\tilde{u}_{2} + \tilde{u}_{3})/2 + c(\rho_{2} - \rho_{3})/(2\rho^{*}),$
 $\rho_{F} = \rho_{2} - (\tilde{u}_{F} - \tilde{u}_{2})\rho^{*}/c$ and

 $S_{F} = S_{4} - (\rho_{F} - \rho_{4})\mathcal{A}/C - (\tilde{u}_{F} - \tilde{u}_{4})\mathcal{B}/C$



$$(\tilde{v}_F - \tilde{v}_1) = 0,$$

$$\rho^* (\tilde{u}_F - \tilde{u}_2) + c (\rho_F - \rho_2) = 0,$$

$$\rho^* (\tilde{u}_F - \tilde{u}_3) - c (\rho_F - \rho_3) = 0 \text{ and }$$

$$\mathcal{A}^*(\rho_F - \rho_4) + \mathcal{B}^*(\tilde{u}_F - \tilde{u}_4) + C^*(S_F - S_4) = 0,$$

along the characteristic wave with speed \tilde{u}^* , along the characteristic wave with speed $\tilde{u}^* + c$, along the characteristic wave with speed $\tilde{u}^* - c$ and along the characteristic wave with speed f'^*/ϕ ,

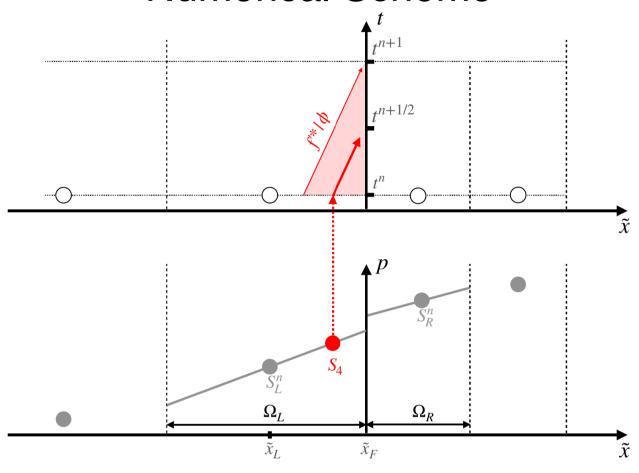
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S_{F} = S_{4} - (\rho_{F} - \rho_{4})\mathcal{A}/C - (\tilde{u}_{F} - \tilde{u}_{4})\mathcal{B}/C$$

$$\mathcal{A} = (c - \tilde{u}^{*})(c + \tilde{u}^{*})S^{*}\phi^{2} + (S^{*}f'^{*}\tilde{u}^{*} - c^{2}f_{1}^{*} + f^{*}\tilde{u}^{*})\phi + f^{*}f'^{*},
\mathcal{B} = (f_{12}^{*}g_{x} - S^{*}f'^{*})\rho^{*}\phi - f'^{*}f_{1}^{*}\rho^{*} \text{ and}
C = (c - \tilde{u}^{*})(c + \tilde{u}^{*})\rho^{*}\phi^{2} + 2f'^{*}\phi\rho^{*}\tilde{u}^{*} - f'^{*}f'^{*}\rho^{*}.$$







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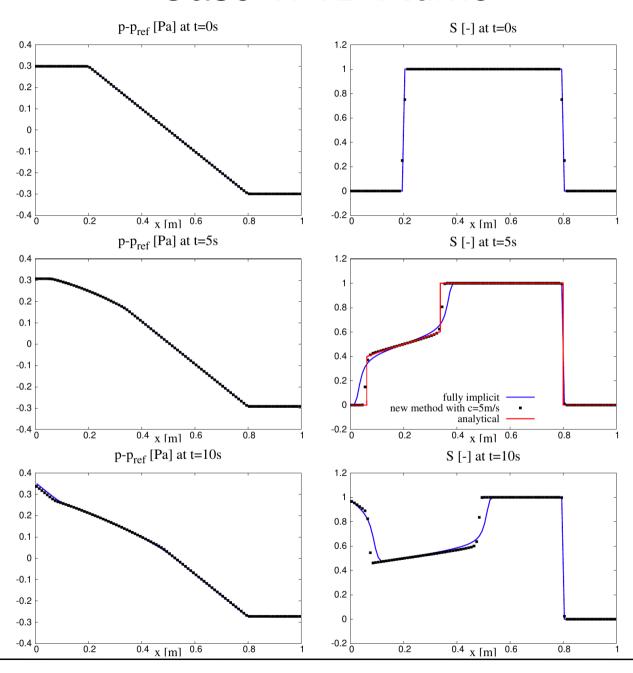
 $C = (c - \tilde{u}^{*})(c + \tilde{u}^{*})\rho^{*}\phi^{2} + 2f'^{*}\phi\rho^{*}\tilde{u}^{*} - f'^{*}f'^{*}\rho^{*}.$

$$\mathcal{A} = (c - \tilde{u}^*)(c + \tilde{u}^*)S^*\phi^2 + (S^*f'^*\tilde{u}^* - c^2f_1^* + f^*\tilde{u}^*)\phi + f^*f'^*,$$

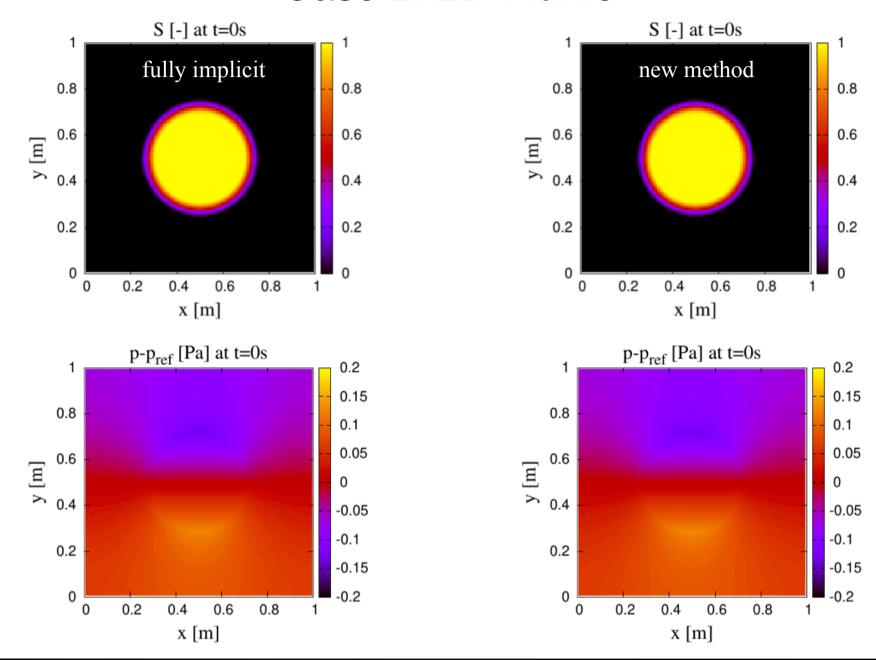
$$\mathcal{B} = (f_{12}^*g_x - S^*f'^*)\rho^*\phi - f'^*f_1^*\rho^* \text{ and}$$

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Case 1: 1D Plume



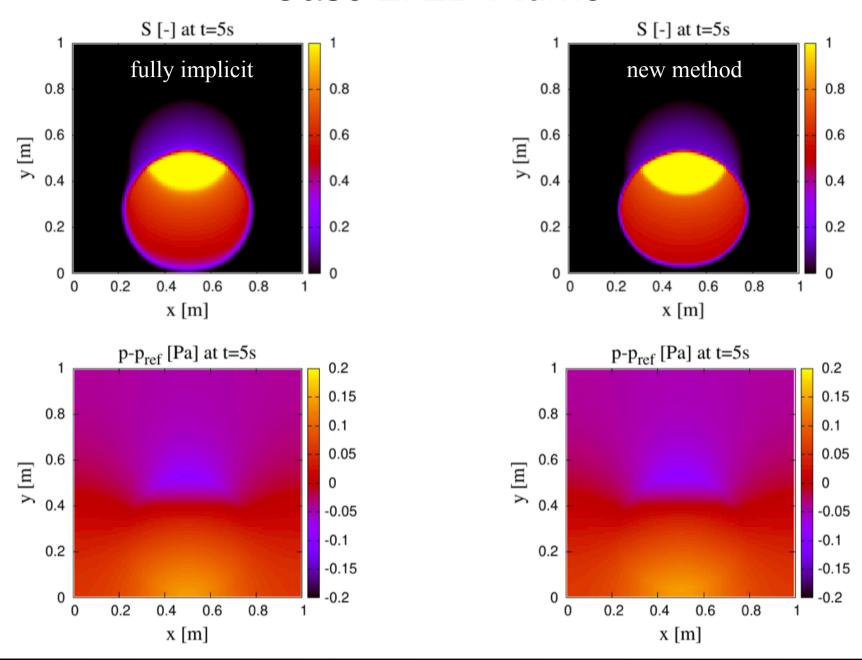
Case 2: 2D Plume







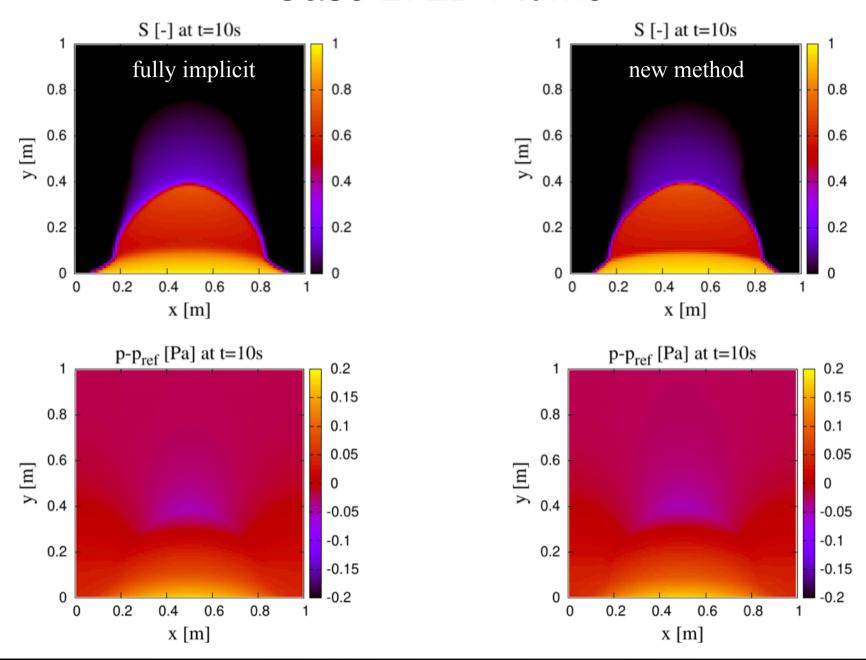
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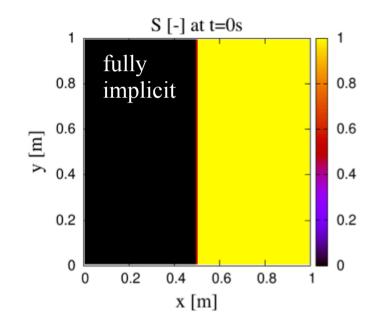
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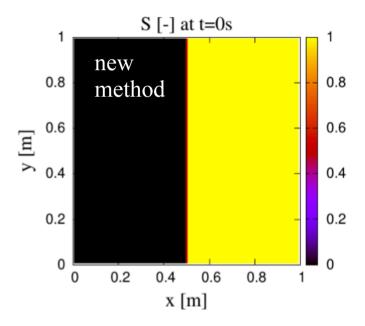






Case 3: Lock Exchange

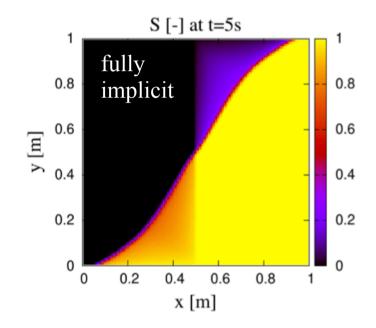


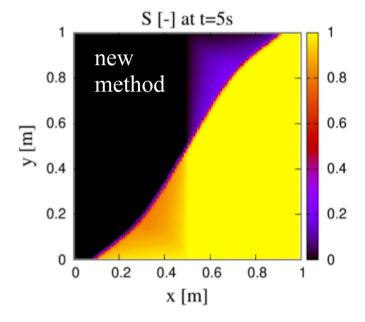






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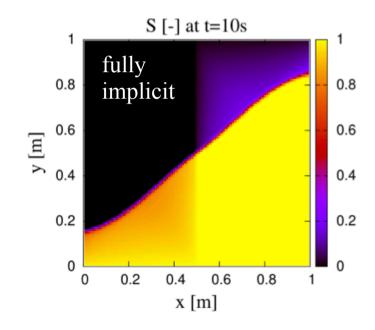


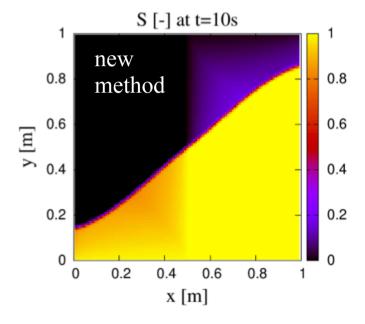


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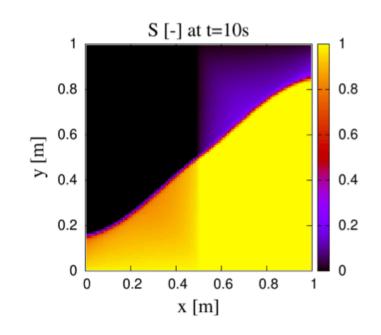
Case 3: Lock Exchange

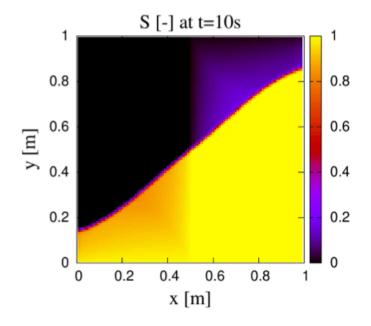






Efficiency





		case 1	case 2	case 3
		(time steps)	(time steps)	(time steps)
fully implicit	1st order	100	1000	1000
new method with $\{c = 1 \text{m/s}, \rho_{mean} = 4 \text{kg/m}^3\}$	1st order		2075	2124
	2nd order	1001	5213	5328
new method with $\{c = 5\text{m/s}, \rho_{mean} = 1\text{kg/m}^3\}$	1st order		10073	10118
	2nd order	5001	40351	40517



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More details in

Patrick Jenny, Rasim Hasanzade, Hamdi Tchelepi. Tightly Coupled Hyperbolic Treatment of Buoyant Two-Phase Flow and Transport in Porous Media. Submitted to Journal of Computational Physics.





thank you for your attention



