# How simplifying capillary effects can affect the traveling wave solution profiles of the foam flow in porous media

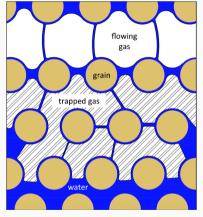
# Grigori Chapiro

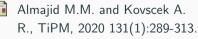
This is a joint work with L. F. Lozano, J. B. Cedro, and R. V. Q. Zavala.

# Foam in porous media

## What is foam in porous media

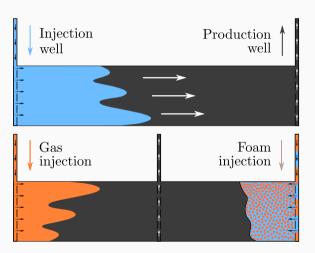
- Lamellae (liquid films) separate gas bubbles.
- Foam reduces the gas mobility.
- Foam texture is modeled as a tracer in the gas phase.
- Foam does not affect water phase relative mobility.



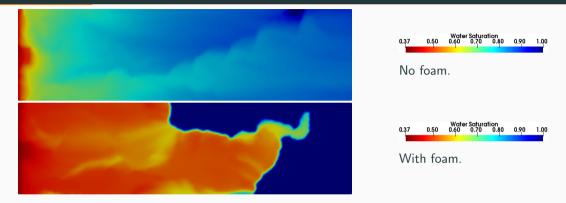


# Applications of foam in porous media

- Soil/aquifer remediation.
- EOR.
- CO<sub>2</sub> sequestration.
- Others.



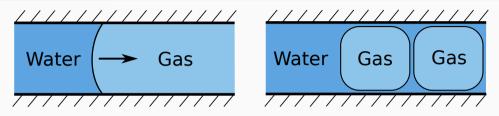
# Two-dimensional simulation in heterogeneous porous media with gravity.



**Figure 1:** Water saturation in SPE10(36) por. medium at time t = 10000s.

F. F. de Paula, T. Quinelato, I. Igreja, G. C., LNCS, 2020.

# How to model foam displacement in porous media



**Figure 2:** Schematic representation of the gas-water flow in a pore throat.

Typical 2-phase flow foam model

$$\int \frac{\partial}{\partial t} \left( \rho_w \phi S_{\mathrm{w}} \right) + \nabla \cdot \left( \rho_w \mathbf{u}_{\mathrm{w}} \right) = 0 \,,$$

$$\frac{\partial}{\partial t} \left( \rho_{g} \phi S_{g} n_{D} \right) + \nabla \cdot \left( \rho_{g} \mathbf{u}_{g} n_{D} \right) = \phi S_{g} \Phi,$$

$$\mathbf{u}_{\mathrm{w}} = \mathbf{u} f_{\mathrm{w}} + \mathbf{k} \lambda_{\mathrm{g}} f_{\mathrm{w}} \nabla P_{\mathrm{c}}$$

Gas phase  $\neq$  Foamed gas

$$\begin{cases} \frac{\partial}{\partial t} \left( \rho_{w} \phi S_{w} \right) + \nabla \cdot \left( \rho_{w} \mathbf{u}_{w} \right) = 0, \\ \frac{\partial}{\partial t} \left( \rho_{g} \phi S_{g} n_{D} \right) + \nabla \cdot \left( \rho_{g} \mathbf{u}_{g} n_{D} \right) = \phi S_{g} \Phi, \\ \mathbf{u}_{w} = \mathbf{u} f_{w} + \mathbf{k} \lambda_{g} f_{w} \nabla P_{c}. \end{cases}$$

$$\begin{cases} \nabla \cdot \left( \rho_{w} \mathbf{u}_{w} \right) = \nabla \cdot \left( \rho_{w} \mathbf{u} f_{w} + \rho_{w} \mathbf{k} \lambda_{g} f_{w} \nabla P_{c} \right), \\ \nabla \cdot \left( \rho_{g} \mathbf{u}_{g} n_{D} \right) = \nabla \cdot \left( \rho_{g} \mathbf{u}_{g} f_{g} n_{D} - \rho_{g} \mathbf{k} \lambda_{g} f_{w} n_{D} \nabla P_{c} \right). \end{cases}$$

Mathematical model

#### First-order kinetic model

Model is composed by conservations laws:

$$\begin{cases} \frac{\partial}{\partial t} \left( \rho_{w} \phi S_{w} \right) + \nabla \cdot \left( \rho_{w} \mathbf{u}_{w} \right) = 0, \\ \frac{\partial}{\partial t} \left( \rho_{g} \phi S_{g} n_{D} \right) + \nabla \cdot \left( \rho_{g} \mathbf{u}_{g} n_{D} \right) = \phi S_{g} \Phi, \\ \mathbf{u}_{w} = \mathbf{u} f_{w} + \mathbf{k} \lambda_{g} f_{w} \nabla P_{c}. \end{cases}$$

#### Assumptions:

- Rigid & homogeneous PM ( $\phi$ , **k** constants);
- Incompressible fluids ( $\rho_{\it w}$ ,  $\rho_{\it g}$  constants);
- Constant injection rate (u is constant);
- One-dimensional case;
- Surfactant amount above CMC.

- Foamed gas relative permeability is reduced by a linear factor (Ashoori et al., 2011):  $\begin{aligned} &\operatorname{MRF}(n_{\mathrm{D}}) = 18500 n_{\mathrm{D}} + 1; \\ &k_{\mathrm{rg}}(S_{\mathrm{w}}, n_{\mathrm{D}}) = \frac{k_{\mathrm{rg}}^{0}(S_{\mathrm{w}})}{\operatorname{MRF}(n_{\mathrm{D}})}. \end{aligned}$
- Linear generation and coalescence rate:  $\Phi = (r_g - r_c) = K_c(n_D^{LE}(S_w) - n_D).$
- Local equilibrium foam texture:

$$n_{
m D}^{
m LE}(S_{
m w}) = egin{cases} anh(A(S_{
m w}-S_{
m w}^*))\,, & S_{
m w} > S_{
m w}^* \ 0 & , & S_{
m w} \leq S_{
m w}^* \end{cases},$$

where  $S_{\rm w}^*$  is the water saturation at the limiting capilary pressure  $P_{\rm c}^*=P_{\rm c}(S_{\rm w}^*)$ .

## Model's simplifications

Original model from Ashoori et al. (2011):

$$\begin{cases} \frac{\partial S_{\mathrm{w}}}{\partial t} + \frac{\partial f_{\mathrm{w}}}{\partial x} = -\frac{\partial}{\partial x} \left( \alpha \, \lambda_{\mathrm{g}} \, f_{\mathrm{w}} \frac{\mathrm{d} P_{\mathrm{c}}}{\mathrm{d} S_{\mathrm{w}}} \frac{\partial S_{\mathrm{w}}}{\partial x} \right), \\ \frac{\partial (S_{\mathrm{g}} \, n_{\mathrm{D}})}{\partial t} + \frac{\partial (f_{\mathrm{g}} \, n_{\mathrm{D}})}{\partial x} = \frac{\partial}{\partial x} \left( \alpha \, n_{\mathrm{D}} \, \lambda_{\mathrm{g}} \, f_{\mathrm{w}} \frac{\mathrm{d} P_{\mathrm{c}}}{\mathrm{d} S_{\mathrm{w}}} \frac{\partial S_{\mathrm{w}}}{\partial x} \right) + \mathcal{K}_{c} \, S_{\mathrm{g}} (n_{\mathrm{D}}^{\mathrm{LE}} - n_{\mathrm{D}}). \end{cases}$$

Define:

$$\epsilon_{
m w} = -lpha\,\lambda_{
m g}\,f_{
m w}\,{
m d}P_{
m c}/{
m d}S_{
m w}, \qquad \epsilon_{
m g} = -lpha\,n_{
m D}\lambda_{
m g}\,f_{
m w}\,{
m d}P_{
m c}/{
m d}S_{
m w}.$$

We consider  $\epsilon_{\rm w}$  and  $\epsilon_{\rm g}$  constants satisfying:

• Simplification 1:

• Simplification 2:

• Simplification 3:

$$\epsilon_{\mathrm{g}} = 0.$$

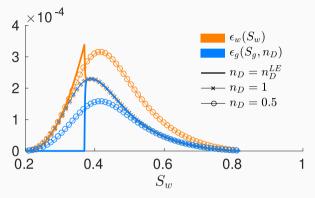
$$\epsilon_{\rm g} = \epsilon_{\rm w}$$
.

$$\epsilon_{\mathrm{g}} = \epsilon_{\mathrm{w}} n_{\mathrm{D}}.$$



Ashoori, E., et al., *Colloids and Surfaces A: Physicochemical and Engineering Aspects*, 377, 228–242, 2011

#### Estimation of constant $\epsilon$



**Figure 3:** Values of  $\epsilon_{\rm w}(S_{\rm w})$  and  $\epsilon_{\rm g}(S_{\rm g}, n_{\rm D})$  for three choices of  $n_{\rm D}$ .

These functions guide us on choosing a constant value for  $\varepsilon_w$  and  $\varepsilon_g$ :

- $\epsilon_{\rm w}$  is up to  $3.387 \cdot 10^{-4}$ ;
- $\bullet$   $\epsilon_{
  m g}$  is up to  $2.299 \cdot 10^{-4}$ ;
- When adopted we assume this constants are equal to  $\epsilon=10^{-4}$ .

# What is a traveling wave solution?

Consider the PDE:

$$\frac{\partial u}{\partial t} - \frac{\partial u}{\partial x} + \frac{\partial F(u)}{\partial x} = \epsilon \Delta_{xx} u + G(u), \qquad u, F(u) \in \mathbb{R}^n.$$

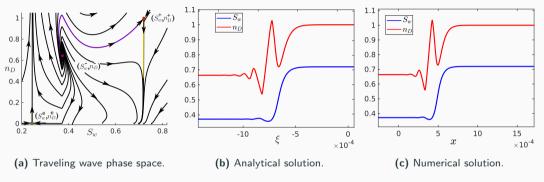
Two (three?) steps:

- (1) Change of variables  $(x, t) \to (\xi, t)$ , where  $\xi = x vt$  with v constant traveling wave velocity,  $\xi$  traveling variable (Euler–Lagrange coordinates)
- (2) Search for the stationary solution of the system

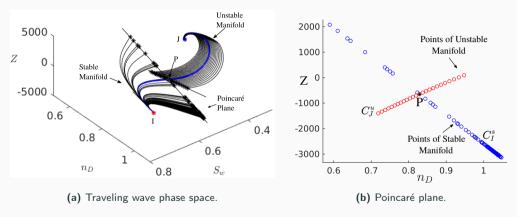
$$\frac{\partial u}{\partial t} - V \frac{\partial u}{\partial \xi} + \frac{\partial F(u)}{\partial \xi} = \epsilon \Delta_{\xi\xi} u + G(u), \qquad u, F(u) \in \mathbb{R}^n.$$

- (3) If we are dealing with the Riemann problem, the solution must satisfy the corresponding asymptotic boundary conditions.
  - A. I. Volpert et al., *AMS*, V. 140, 2000.

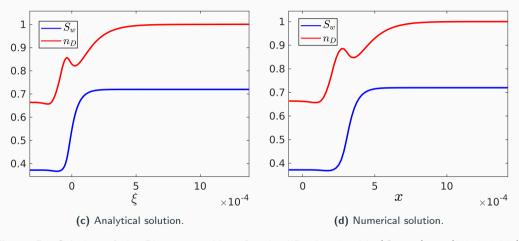
# Results



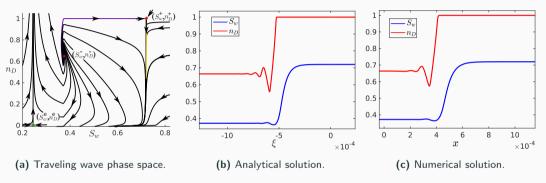
**Figure 4:** Solution of the Riemann problem for simplification 1 with  $(S_{\rm w}^-, n_{\rm D}^-) = (0.372, 0.664)$ ,  $(S_{\rm w}^+, n_{\rm D}^+) = (0.72, 1.0)$ ,  $\epsilon = 10^{-4}$ , and  $K_{\rm c} = 1.0$ .



**Figure 5:** Solution of the Riemann problem for simplification 2 with  $(S_{\rm w}^-, n_{\rm D}^-) = (0.372, 0.664)$ ,  $(S_{\rm w}^+, n_{\rm D}^+) = (0.72, 1.0)$ ,  $\epsilon = 10^{-4}$ , and  $K_{\rm c} = 1.0$ .



**Figure 5:** Solution of the Riemann problem for simplification 2 with  $(S_{\rm w}^-, n_{\rm D}^-) = (0.372, 0.664)$ ,  $(S_{\rm w}^+, n_{\rm D}^+) = (0.72, 1.0)$ ,  $\epsilon = 10^{-4}$ , and  $K_{\rm c} = 1.0$ .



**Figure 6:** Solution of the Riemann problem for simplification 3 with  $(S_{\rm w}^-, n_{\rm D}^-) = (0.372, 0.664)$ ,  $(S_{\rm w}^+, n_{\rm D}^+) = (0.72, 1.0)$ ,  $\epsilon = 10^{-4}$ , and  $K_{\rm c} = 1.0$ .

# Traveling wave solutions for all simplified capillary pressure models

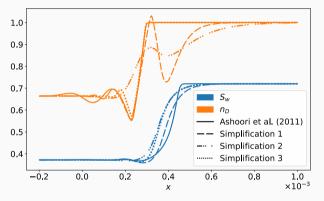


Figure 7: Numerical solution for different models.

- Numerical and analytical solutions match.
- All profiles present oscillations before the wavefront.
- All models present the same wave velocity.
- Simplification 3 is the closest to the original kinetic model.



L. F. Lozano, R. V. Q. Zavala and G. C., *Computational Geosciences*, 25, 515–527, 2021

### **Discussions & Conclusions**

- There should be a difference in modeling two-phase gas-water flow in the presence / absence of foam.
- We analyzed different mathematical simplifications pointing out that the traveling wave profile presents different oscillations.
- We stress that physically acceptable simplification procedures can result in qualitatively inaccurate solutions describing foam texture.
- We wonder whether this phenomenon can be observed in laboratory experiments.



L. F. Lozano, J. B. Cedro, R. V. Q. Zavala and G. C., *International Journal of Non-Linear Mechanics*, 139, p. 103867, 2022

# Thank you for attention!



Questions?



Laboratory of Applied Mathematics www.ufjf.br/lamap







